

# Standalone Mode of Power Generation using Micro Wind Energy System

<sup>1</sup>S.Rajkumar, PhD Scholar, AMET University, Kanathur , Chennai-600135, email id : srajece@gmail.com

<sup>2</sup>K.Gugan, PhD Scholar, AMET University, Kanathur , Chennai-600135, email id : kgugan@ymail.com

<sup>3</sup>Lalysaman, Assistant professor, VeermataJijabai Technological Institute , Mumbai, India email Id: laly\_89@yahoo.co.in

<sup>[1,2,&3]</sup>Department of Electrical and Electronics Engineering

**Abstract-** In the miniaturized scale matrix organize, it is especially difficult to reinforce the heap without consistent power supply. The proposed miniaturized scale wind vitality transformation framework with battery imperativeness stockpiling is used to exchange the controllable honest to goodness and responsive power in the lattice and to keep up the power quality at the reason for conventional coupling. The created smaller scale wind power can be expelled under fluctuating wind speed and can be secured in the batteries at low power ask for hours. In this arrangement, inverter control is executed with hysteresis current control mode to achieve the speedier element switchover for the support of load. The mix of battery stockpiling with small scale wind vitality era framework ( $\mu$ WEGS), which will join the yield waveform by imbuing or charming responsive power and engage the bona fide control stream required by the heap. The framework diminishes the weight on the ordinary source and uses small scale wind vitality era framework ( $\mu$ WEGS) and battery stockpiling power under load limitations. The framework gives quick response to reinforce the heap. The arrangement can in like manner be functioned as a remain solitary framework in

case of network disappointment like a constant power supply.

## INTRODUCTION

Extensive wind ranches have been presented in power frameworks around the world in light of characteristic issues brought on by using fossil vitality assets. The advancement rate of overall presented wind control point of confinement was around 30% for each annum in the latest decade. High renewable power penetration impacts affects framework dependability and unwavering quality due to the spasmodic and unverifiable characteristics of wind speed. High populace development and money related progression on the planet, there is an appeal for vitality. As a renewable vitality, wind vitality period has been locked in as a spotless and unending vitality giving a doable answer for vitality lack. The miniaturized scale wind control era framework with battery vitality stockpiling is ending up being more unmistakable with the growing enthusiasm of force era. It furthermore reduces nature pollution. Wind essentialness has exhibited a quick improvement as a flawless and boundless vitality source all around the world. In any case, as the passage levels

increase, it is of broad stress that a fluctuating power yield of wind farms will impact operation of interconnected cross sections, especially weak power framework. Such cases may require a couple measures to smooth the yield fluctuation to have a trustworthy power system. Late advances in electric vitality stockpiling innovations give a chance of utilizing vitality stockpiling to address the wind vitality discontinuity.

### **A. Battery stockpiling**

Electric vitality can be put away electromagnetically, electrochemically, dynamically, or as potential vitality. Two components describe the utilization of a vitality stockpiling innovation.

1. Amount of vitality that can be put away in the gadget according to the wind control .
2. Rate at which vitality can be moved into or out of the capacity gadget.

These components depend for the most part on the normal for the capacity gadget itself. An assortment of capacity advances are accessible, which are equipped for smoothing out the unusual fluctuating force yield of the wind ranches. The battery stockpiling is utilized for basic load applications as it supplies control for a brief timeframe. The mix of battery vitality stockpiling and small scale wind creating framework in appropriated control framework can give the compelling, solid, and sturdy power framework. The framework likewise gives vitality sparing and un-interruptible power inside dissemination organize. The parallel handling of wind vitality creating

framework and battery stockpiling will improve the power stream in the conveyed network. The quick reaction normal for the battery vitality stockpiling framework makes stockpiling particularly profitable as a direction asset and empowers it to make up for the fluctuation of wind power era. Battery vitality stockpiling frameworks can likewise enhance the financial aspects of dispersed wind control era by diminished requirement for cycle customary era resources and expanding resource use of existing utility era by permitting the coupled miniaturized scale wind turbine and battery vitality stockpiling framework to give recurrence and voltage direction benefit. The battery bank comprises of numerous batteries associated in a mix arrangement parallel design to give the sought power and vitality capacities for the application

### **B. Small scale wind control**

However the yield force of small scale wind generator is fluctuating and will influence the operation in the circulation arrange. The utility framework can't acknowledge new era without strict state of voltage direction because of genuine power change and responsive power era ingestion. The modern and business clients regularly work the touchy electronic types of gear or basic load that can't endure voltage hangs, voltage swells, or loss of force, which besides cause intrusion in life working types of gear or stoppage in mechanical generation. This requires some measure to alleviate the yield change to keep the power quality in the appropriated network. The small scale wind vitality creating framework is utilized to charge the battery as and when the wind power is accessible. The battery stockpiling gives a fast reaction to either

charging/releasing the battery furthermore goes about as a consistent voltage hotspot for the basic load in the dispersed system. Keeping in mind the end goal to check the adequacy of proposed framework, the present control method of voltage source inverter is proposed to interface the battery stockpiling with small scale wind vitality generator into the circulated organize.

The control framework with battery stockpiling has the accompanying destinations:

1. Unity power component and power quality at the purpose of basic coupling transport.
2. Real and responsive power bolster from wind generator and batteries to the heap .
3. Stand-alone operation in the event of network disappointment.

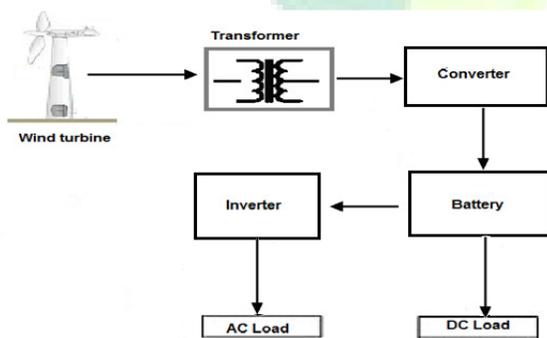


Figure 1.1:Block chart for wind control framework

Fig. 1.1 demonstrates the square graph for the wind control generation through a miniaturized scale wind turbine and smaller scale inverter to the yield terminal when the

framework is associated with the lattice. At the point when establishment of the air conditioner module is occurring; this potential contrast could posture dangers to both the laborer and the offices. A drifting dynamic change is intended to disconnect the dc current from the converter. The plan keeps up solidarity control consider furthermore consonant free source current at the purpose of basic association in the circulated arrange. It permits the genuine power stream amid the momentary request of the heap. The control for fast infusion or retention of responsive/genuine power stream in the power framework is conceivable. This plan is gives the framework to work in power quality mode.

The paper propose the small scale wind vitality change conspire with battery vitality stockpiling, with an interface of inverter in current controlled mode for trade of genuine and receptive power support to the basic load. The hysteresis current controller is utilized to produce the exchanging signal for inverter in a manner that it will wipe out the symphonious current in the framework. The trading of force is directed over the dc transport having vitality stockpiling and is made accessible under the unfaltering state condition. This likewise permits the genuine power stream amid the immediate request of the heap. This plan is giving framework works not just in power quality mode and in addition in a lattice associated mode.

### C. Wind Power Extraction with Batteries

The proposed smaller scale wind vitality extraction from wind generator and battery vitality stockpiling with dispersed

system is designed on its working guideline and depends on the control technique for exchanging the inverter for basic load application as appeared in Fig 1.2.

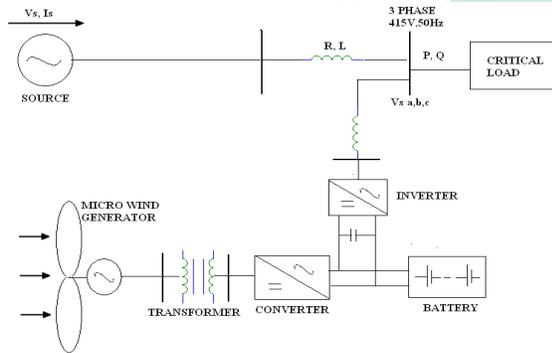


Figure 1.2: Scheme of smaller scale twist generator with battery stockpiling for basic load application

The smaller scale wind producing framework ( $\mu$ WEGS) is associated with turbine, acceptance generator, interfacing transformer, and air conditioning dc converter to get dc transport voltage. The power stream is spoken to with dc transport current for steady dc transport voltage in inverter operation. The static normal for wind turbine can be portrayed with the relationship in the twist as in

$$P_{\text{wind}} = \frac{1}{2} \rho \pi R^2 (V_{\text{wind}})^3 \quad (1.1)$$

where,

$\rho$  - air thickness (1.225 kg/m<sup>3</sup>),

R-rotor sweep in meters,

VWIND - twist speed in m/s.

It is unrealistic to concentrate all motor vitality of wind and is called CP control coefficient. This power coefficient can be

communicated as a component of tip speed proportion  $\lambda$  and pitch edge  $\theta$ .

The mechanical power can be composed as

$$P_{\text{mech}} = C_P * P_{\text{wind}} \quad (1.2)$$

$$P_{\text{mech}} = C_P * \frac{1}{2} \rho \pi R^2 (V_{\text{wind}})^3 \quad (1.3)$$

By using the turbine rotational speed,  $\omega_{\text{turbine}}$  mechanical torque is shown in

$$T_{\text{mech}} = (P_{\text{mech}}) / \omega_{\text{turbine}} \quad (1.4)$$

The power in the wind is relative to the 3D shape of the wind speed. Be that as it may, just part of the wind power is extractable. In spite of the fact that an entire streamlined model of the wind turbine could reenact the association between the wind and the turbine sharp edges in detail, the basic articulation of (1.3), which is frequently used to portray the mechanical power transmitted to the center point shaft.

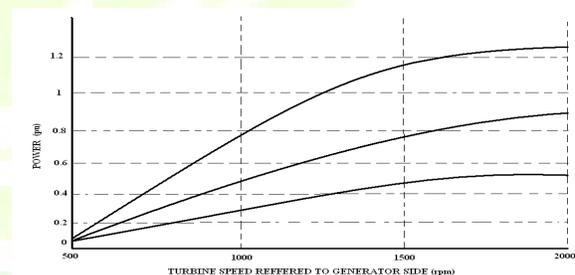


Figure 1.3: Power-speed normal for turbine

#### D. DC Link for Battery Storage and Micro - Wind Energy Generator

The battery stockpiling and  $\mu$ WEGS are associated over the dc connect as appeared in Fig. 1.4. The dc interface comprises of capacitor which decouples the  $\mu$ wind

producing framework and air conditioning source (matrix) framework.

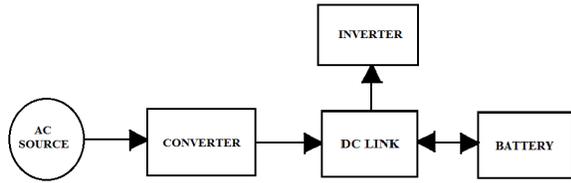


Figure 1.4: Block chart of DC connection framework

The battery stockpiling will get accused of the assistance of  $\mu$ wind generator. The utilization of capacitor in dc connection is more effective, less costly and is demonstrated as takes after:

$$C \frac{d}{dt}(V_{dc}) = I_{dc(rect)} I_{dc(inv)} - I_b \quad (1.5)$$

where,

$C$  = dc connect capacitance,

$V_{dc}$  = rectifier voltage,

$I_{dc(rect)}$  = redressed dc-side current,

$I_{dc(inv)}$  = inverter dc-side current,

$I_b$  = battery current.

The battery stockpiling is associated with dc connect and is spoken to by a voltage source  $E_b$  connected in arrangement with an inner resistance  $R_b$ . The interior voltage differs with the charged status of the battery. The terminal voltage  $V_{dc}$  is given in

$$V_{dc} = E_b - (I_b * R_b) \quad (1.6)$$

It is important to keep sufficient dc connect level to meet the inverter voltage as in

$$V_{dc} \geq \frac{2\sqrt{2}}{Ma} V_{inv} \quad (1.7)$$

where ,

$V_{inv}$  = line-to-nonpartisan rms voltage of inverter

(240 Vrms),

$f$  = inverter yield recurrence 50 Hz,

$Ma$  = adjustment file.

Along these lines, the dc connection is intended for 800V.

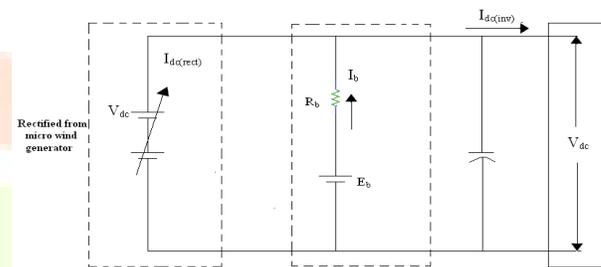


Figure 1.5: DC connect for battery stockpiling and microwind generator.

## 2.CONTROL SCHEME OF THE SYSTEM

The control plot with battery stockpiling and miniaturized scale wind producing framework uses the dc connection to extricate the vitality from the wind. The small scale wind generator is associated through a stage up transformer and to the rectifier connect in order to acquire the dc transport voltage. The battery is utilized for keeping up the dc transport voltage consistent; in this way the inverter is executed effectively in the circulated framework. The three-leg 6-beat inverter is interfaced in disseminated arrange and double mix of battery stockpiling with small

scale twist generator for basic load application, as appeared in Fig. 2.1.

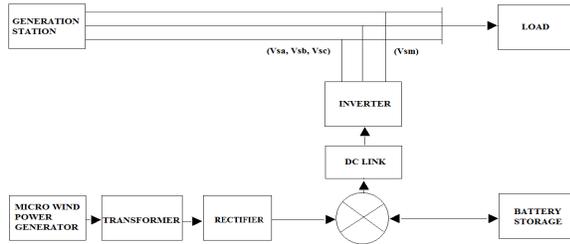


Figure 2.1: Inverter interface with mix of battery stockpiling with  $\mu$ WEGs.

The control plot approach depends on infusing the current into the framework utilizing "hysteresis current controller." Using such methods the controller keeps the control framework factors between the limits of hysteresis range and gives rectify exchanging signals for inverter operation.

### A. Network Synchronization

In the three-stage adjust framework, the RMS voltage source adequacy is computed at the testing recurrence from the source stage voltage ( $V_{sa}$ ,  $V_{sb}$ ,  $V_{sc}$ ) and is communicated as test format  $V_{sm}$ , as in

$$V_{sm} = \left\{ \frac{2}{3} (V_{sa}^2 + V_{sb}^2 + V_{sc}^2) \right\}^{1/2} \quad (2.1)$$

The in-stage unit vectors are acquired from air conditioning source-stage voltage and the RMS estimation of unit vector  $U_{sa}$ ,  $U_{sb}$ ,  $U_{sc}$  as appeared in

$$U_{sa} = \frac{V_{sa}}{V_{sm}} ; \quad U_{sb} = \frac{V_{sb}}{V_{sm}} ; \quad U_{sc} = \frac{V_{sc}}{V_{sm}} \quad (2.2)$$

The unit vector executes the essential capacity in the matrix for the synchronization of inverter. This strategy is

straightforward, vigorous and good as contrasted and different strategies.

### B. Hysteresis Based Current Controller

Hysteresis based current controller is executed in the present control conspire. The reference current is created and the real current is identified by current sensors that are subtracted for getting present blunders for a hysteresis based controller. The ON/OFF exchanging signals for IGBT of inverter are gotten from hysteresis controller. At the point when the genuine (measured) current is higher than the reference current, it is important to commutate the relating switch to get negative inverter yield voltage. This yield voltage diminishes the yield current and achieves the reference current.

On other hand, if the deliberate current is not exactly the reference current, the change commutated to acquire a positive inverter yield voltage. Hence the yield current increments and it goes to the reference current. Thus, the yield current will be inside a band around the reference one. The present control method of inverter infuses the current into the lattice in a manner that the source streams are sans consonant and their stage points are in-stage as for source voltage. Consequently, the infused current will counteract the receptive and symphonious piece of load current. The control exchange happens when battery vitality framework is completely accused of the assistance of smaller scale wind generator. To accomplish this objective, the source voltage is detected and synchronized in creating the craved reference current summon for the inverter operation. The usage of the hysteresis band current control

is not costly. The control is great for a quick reaction of an inverter to fast changes of reference current, since current control has immaterial inactivity and deferral.

Along these lines the fundamental benefits for the controlling modes are the accompanying

1. Provide symphonious free source current
2. Cancels the responsive piece of load current
3. Provide quick reaction to framework

C. Variable speed idea of miniaturized scale wind turbine

In a variable-speed turbine with doubly sustained enlistment turbine, the converter nourishes the rotor winding, while the stator winding is associated specifically to the framework. This converter, thus decoupling mechanical and electrical frequencies and making variable-speed operation conceivable, can shift the electrical rotor frequency. This turbine can't work in the full range from zero to the appraised speed, however the speed range is very sufficient. This restricted speed range is brought on by the way that a converter that is impressively littler than the evaluated force of the machine is utilized. On a basic level, one can state that the proportion between the size of the converter and the wind-turbine rating is half of the rotor-speed traverse. Notwithstanding the way that the converter is smaller, the misfortunes are likewise lower. The control potential outcomes of the reactive power are like the full power-converter framework.

### 3. FRAMEWORK PERFORMANCE AND RESULTS

The plan of miniaturized scale twist generator with battery vitality stockpiling for extraction of twist vitality for basic load application is appeared in Fig. 3.2 and is reproduced in MATLAB/SIMULINK with power framework square set. A simulink show library incorporates the model of converter, enlistment generator, basic load, and others that has been developed for reenactment. The reenactment parameters for the given framework are given in Table 3.1.

Source voltage	3 – phase ,415V, 50Hz
Source and line inductance	0.5Mh
Micro wind generator parameter (induction generator)	150kW, 415V, 50Hz, P = 4, $R_s = 0.01\Omega$ , $R_r = 0.015m\Omega$ , $L_s = 0.06H$ , $L_r = 0.06H$ , wind velocity ( $\theta$ ) = 5m/s
DC link parameter	DC link = 800V, C = 5Mf
Rectifier – bridge parameter (three arm bridge type)	Snubber R = 100 $\Omega$ , $R_{on} = 0.01\Omega$ , snubber capacitor = $0.01e^{-3}F$
IGBT device parameter (three arm bridge type)	Rated voltage 1200V, Forward current 50A, Gate voltage +/-20V, turn-ON 70ns delay, turns-OFF delay 400ns, Power dissipation 300W
Battery parameters	DC 800V, cell capacity 500Ah, Type – Lead acid
Interfacing transformer	Rating – 1KVA, Y-Y type, 415/800V, 50Hz
Critical load parameter	3– phase 415V, non linear load, R = 10 $\Omega$ , C = 1 $\mu F$

Table 3.1: System Parameters

### A. Execution of battery stockpiling

The miniaturized scale wind vitality generator is worked to produce the power and is provided to uncontrolled rectifier to interface the dc connect. The battery model is considered as it gets charged independently in order to take the upside of wind source. This coordination is made physically in the reenactment of the framework. To exchange the genuine power from twist generator into the heap, the produced power is nourished to rectifier for charging the batteries. The corrected current from wind generator and battery stockpiling is in figure underneath.

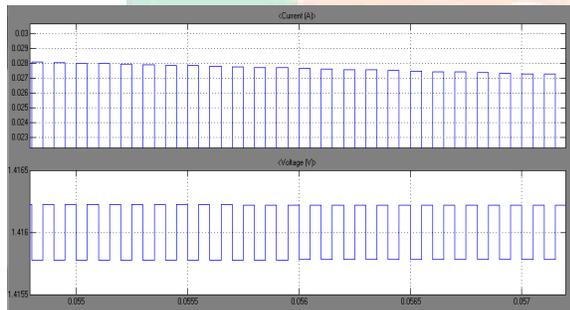


Figure 3.2: Voltage and Current in Battery stockpiling

### B. Execution of Micro Wind Energy System

The normal power stream for the proposed framework can be observed for dynamic and receptive power stream (P,Q) as appeared in figure beneath. The normal power stream is measured at the purpose of regular coupling, with and without controller operation in the lattice. The controller is worked for power quality mode to infuse the power at amid this operation source responsive power is

diminished to zero, as it is upheld from the inverter amid power quality mode.

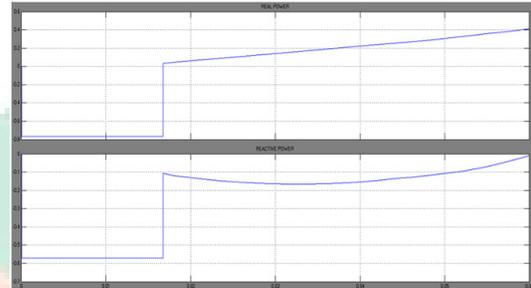


Figure 3.3: Real power and Reactive force of  $\mu$ WES

### C. Execution under remain solitary mode

The miniaturized scale wind generator is worked as a remain solitary mode and amid this mode the source current is zero. In this mode just the inverter will bolster the requested dynamic and receptive power-bolster for the basic load and line misfortunes as the matrix supply is not accessible in such method of operation. The plan for basic load application has control quality change as well as backings the basic load with the vitality stockpiling through the batteries. In this manner we get a sinusoidal yield from the heap side under remain solitary condition as appeared in figure underneath.

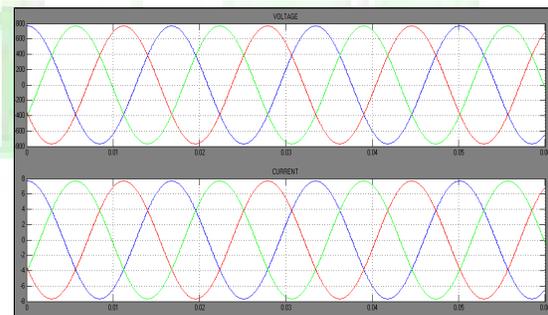


Figure 3.4 : Load voltage and Load current

#### 4. CONCLUSION

The miniaturized scale wind vitality transformation plot with battery vitality stockpiling, with an interface of inverter is utilized for trade of genuine and responsive power support to the heap. The hysteresis current controller is utilized to produce the exchanging signal for inverter in a manner that it will cross out the consonant current in the framework. The plan keeps up a superior component furthermore symphonious free source current at the purpose of regular association in the circulated arrange. The trading of wind power is controlled over the dc transport having vitality stockpiling and is made accessible under the consistent state condition. This likewise permits the genuine power stream amid the quick request of the heap. The proposed control framework is suited for fast infusion or ingestion of responsive/genuine power stream in the power framework. The battery vitality stockpiling gives quick reaction and upgrades the execution under the change of wind turbine yield and enhances the voltage security of the framework. This plan is giving a decision to choose the genuine power for the heap, among the accessible wind-battery-ordinary assets and the framework works in power quality mode and in a remain solitary mode.

#### REFERENCES

1. B. Singh, S. S. Murthy, and S. Gupta, "Analysis and design of STATCOM-based voltage regulator for self-excited induction generator," *IEEE Trans. Energy Conversion*, vol. 19, no. 4, pp. 783–791, Dec. 2004.
2. A. D. Patton, C. Singh, and M. Sahinoglu, "Operating considerations generation reliability modeling-an analytical approach," *IEEE Trans. Power App. Syst.*, vol. PAS-100, pp. 2656–2663, May 1981.
3. A. M. L. da Silva, W. S. Sales, L. A. da Fonseca Manso, and R. Billinton, "Long-term probabilistic evaluation of operating reserverequirements with renewable sources," *IEEE Trans. Power Syst.*, vol. 25, no. 1, pp. 106–16, Feb. 2010.
4. C. Singh and Y. Kim, "An efficient technique for reliability analysis of power systems including time dependent sources," *IEEE Trans. Power Syst.*, vol. 3, no. 3, pp. 1090–1096, Aug. 1988.
5. D. Graovac, V. A. Katic, and A. Rufer, "Power quality problems compensation with universal power quality conditioning system," *IEEE Trans. Power Delivery*, vol. 22, no. 2, pp. 968–997, Apr. 2007.
6. F. S. Pai and S.-I. Hung, "Design and operation of power converter for microturbine powered distributed generator with capacity expansion capability," *IEEE Trans. Energy Conversion*, vol. 3, no. 1, pp. 110–116, Mar. 2008.
7. G. Strbac, A. Shakoob, M. Black, D. Pudjianto, and T. Bopp, "Impact of wind generation on the operation and development of the UK electricity systems," *Elect. Power Syst. Res.*, vol. 77, pp. 1214–1227, Jul. 2007.
8. G. Tapia, "Proportional-integral regulator based application to wind farm reactive power management for secondary voltage control," *IEEE Trans. Energy Conversion*, vol. 22, no. 2, pp. 488–498, Jun. 2007.

9. Global Wind 2005 Report, Global Wind Energy Council(GWEC). [Online]. Available: <http://www.gwec.net>.
10. J. M. Carrasco, "Power-electronic system for grid integration of renewable energy source: A survey," *IEEE Trans. Ind. Electron.*, vol. 53, no. 4, pp. 1002–1014, Jun. 2006.
11. L. Maharjan, S. Inoue, H. Akagi, and J. Asakur, "State-of-charge (SoC)-balancing control of a battery energy storage system based on a cascade PWM converter," *IEEE Trans. Power Electron*, vol. 24, no. 6, pp. 1628–1636, Jun. 2009.
12. L. Wang and C. Singh, "Population-based intelligent search reliabilityevaluation of generation systems with wind power penetration," *IEEE Trans. Power Syst.*, vol. 23, no. 3, pp. 1336–1345, Aug. 2008.
13. M. A. Ortega-Vazquez and D. S. Kirschen, "Estimating the spinningreserve requirements systems with significant wind power generationpenetration," *IEEE Trans. Power Syst.*, vol. 24, no. 1, pp. 114–124, Feb. 2009.
14. M. A. Ortega-Vazquez and D. S. Kirschen, "Optimizing the spinningreserve requirements using a cost/benefit analysis," *IEEE Trans. PowerSyst.*, vol. 22, no. 1, pp. 24–33, Feb. 2007.
15. M. Matos and J. P. Lopes *et al.*, "Probabilistic evaluation of reserverequirements of generating systemswith renewable power sources: ThePortuguese and Spanish cases," *Int. J. Elect. Power Energy Syst.*, vol.31, no. 9, pp. 562–569, Oct. 2009.
16. P. C. Loh, M. J. Newman, D. N. Zmood, and D. G. Holmes, "A comparative analysis of a multiloop voltage regulation strategies for single and three phase UPS system," *IEEE Trans. Power Electron*, vol. 18, no. 5, pp. 1176–1185, Sep. 2003.
17. R. Billinton and A. A. Chowdhury, "Incorporation of wind energyconversion systems conventional generating capacity adequacy assessment," *Proc. Inst. Elect. Eng., Gen., Transm.,Distrib.*, vol. 139, no. 1, pp. 47–56, Jan. 1992.
18. R. Billinton and Bagen, "Incorporating reliability index distributionssmall isolated generating system reliability performance assessment," *Proc. Inst. Elect. Eng., Gen., Transm.,Distrib.*, vol. 151, no. 4, pp.469–476, Jul. 2004.
19. R. Billinton and G. Bai, "Generating capacity adequacy associatedwith wind energy," *IEEE Trans. Energy Convers.*, vol. 19, no. 3, pp.641–646, Sep. 2004.
20. R. Billinton and H. Chen, "Assessment of risk-based capacity benefitfactors associated with wind energy conversion systems," *IEEE Trans.Power Syst.*, vol. 13, no. 3, pp. 1191–1196, Aug. 1998.
21. R. Billinton and R. Karki, "Capacity expansion of small isolated powersystems using PV and wind energy," *IEEE Trans. Power Syst.*, vol. 16,no. 4, pp. 892–897, Nov. 2001.
22. R. Billinton and R. N. Allan, *Reliability Evaluation of Power Systems*. New York: Plenum, 1996.
23. R. Billinton, B. Karki, and R. Karkiet *al.*, "Unit commitment risk analysisof wind integrated power systems," *IEEE Trans. Power Syst.*, vol.24, no. 2, pp. 930–939, May 2009.

24. S. T. Lee and Z. A. Yamayee, "Load-following and spinning-reserve penalties for intermittent generation," *IEEE Trans. Power App. Syst.*, vol. PAS-100, no. 3, pp. 1203–11, Mar. 1981.
25. S. Teleke, M. E. Baran, A. Q. Huang, S. Bhattacharya, and L. Anderson, "Control strategy for battery energy storage for wind farms dispatching," *IEEE Trans Energy Conversion*, vol. 24, no. 3, pp. 725–731, Sep. 2009.
26. S. W. Mohod and M. V. Aware, "A STATCOM-control scheme for grid connected wind energy system for power quality improvement," *IEEE Syst. J.*, vol. 2, no. 3, pp. 346–352, Sep. 2010.
27. S. W. Mohod and M. V. Aware, "Power quality issues and its mitigation technique in wind energy conversion," in *Proc. IEEE ICQPH*, Sep.–Oct. 2008, pp. 1–6.
28. W. Wangdee and R. Billinton, "Considering load-carrying capability and wind speed correlation of WECS generation adequacy assessment," *IEEE Trans. Energy Convers.*, vol. 21, no. 3, pp. 734–741, Sep. 2006.
29. Y. Chauhan, S. Jain, and B. Sing, "Static volt-ampere reactive compensator for self-excited induction generator feeding dynamic load," *Electric Power Compon. Syst. J.*, vol. 36, no. 10, pp. 1080–1101, Oct. 2008.
30. Z. Chen and E. Spooner, "Grid power quality with variable speed wind turbines," *IEEE Trans. Energy Conversion*, vol. 16, no. 2, pp. 148–154, Jun. 2008.
31. Z. Jiang, "Adaptive control strategy for active power sharing in hybrid fuel cell/battery power source," *IEEE Trans. Energy Conversion*, vol. 22, no. 2, pp. 507–515, Jun. 2007.
32. Z. Yang, C. Shen, and L. Zhang, "Integration of stat COM and battery energy storage," *IEEE Trans. Power Syst.*, vol. 16, no. 2, pp. 254–262, May 2001.

IJARMATE